## Real Time Stepper Motor Linear Ramping Just by Addition and Multiplication

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## 1. Kinematic basics

The linear acceleration (ramping) formulas are:

$$
\begin{gathered}
\mathbf{S}=\mathbf{v}_{0} \cdot \mathbf{t}+\mathbf{a} \cdot \mathbf{t}^{2} / \mathbf{2} \\
\mathbf{v}=\mathbf{v}_{0}+\mathbf{a} \cdot \mathbf{t}
\end{gathered}
$$

where
S - acceleration distance, in stepper motor case - number of steps,
$\mathbf{v}_{0}$ - initial velocity, base speed (steps per second),
v - target velocity, slew speed (steps per second),
a - acceleration (steps per second per second),
t - acceleration time, ramping period (seconds).
By rearranging [

$$
t=\left(v-v_{0}\right) / a
$$

and putting it in [1] we have

$$
\begin{equation*}
S=\left(v^{2}-v_{0}^{2}\right) /(2 \cdot a) \tag{4}
\end{equation*}
$$

and

$$
\begin{equation*}
v=\left(v_{0}^{2}+2 \cdot a \cdot S\right)^{1 / 2} \tag{5}
\end{equation*}
$$

that can be represented as a recursive form of speed calculation for one step:

$$
\begin{equation*}
v_{i}=\left(v_{i-1}^{2}+2 \cdot a\right)^{1 / 2} \tag{6}
\end{equation*}
$$

where
i - step number $(1 \leq \mathbf{i} \leq \mathbf{S})$.

## 2. Control basics

To produce the speed profile for stepper motor we need to provide the real time delays between step pulses:

$$
\begin{equation*}
p_{i}=F / v_{i} \tag{7}
\end{equation*}
$$

where
$\mathbf{p}_{\mathbf{i}}$ - delay period for the $\mathbf{i}$-th step (timer ticks),
F - timer frequency (count of timer ticks per second),
so according to [6] the exact delay value will be:

$$
\begin{equation*}
p_{i}=F /\left(\left(F / p_{i-1}\right)^{2}+2 \cdot a\right)^{1 / 2} \tag{8}
\end{equation*}
$$

or

$$
\begin{equation*}
p_{i}=p_{i-1} /\left(1+p_{i-1}^{2} \cdot 2 \cdot a / F^{2}\right)^{1 / 2} \tag{9}
\end{equation*}
$$

## 3. Approximation

Using Taylor series

$$
1 /(1+n)^{1 / 2} \simeq 1-n / 2
$$

when $-1<\mathbf{n} \leq 1$ we can approximate [9] to

$$
\begin{equation*}
p_{i}=p_{i-1} \cdot\left(1-p_{i-1}^{2} \cdot a / F^{2}\right) \tag{11}
\end{equation*}
$$

Let's check the $-1<\mathbf{n} \leq 1$ condition. Our $\mathbf{n}$ was

$$
\mathbf{n}=\mathbf{p}_{\mathrm{i}-1}^{2} \cdot \mathbf{2} \cdot \mathbf{a} / \mathrm{F}^{2}
$$

or, by velocity,

$$
\begin{equation*}
n=2 \cdot a / v_{i-1}^{2} \tag{13}
\end{equation*}
$$

The maximum $\mathbf{n}$ value will be at minimum speed, on the first calculated step, where $\mathbf{i}=2$

$$
\mathbf{n}_{\max }=\mathbf{2} \cdot \mathbf{a} / \mathbf{v}_{1}{ }^{2}
$$

Because the minimal $\mathbf{v}_{0}$ is 0 , from [6] we have

$$
\begin{equation*}
v_{1 \text { min }}=(2 \cdot a)^{1 / 2} \tag{15}
\end{equation*}
$$

So $\mathbf{n}$ will be always less than or equal to 1. Because our calculations are forward-only we have no limitation in case of deceleration (negative acceleration) too.

## 4. Implementation

The given parameters are:
$\mathbf{v}_{0}$ - base speed,
v - slew speed,
a - acceleration,
F - timer frequency
and the calculated parameters are:
S - acceleration/deceleration distance

$$
\mathbf{S}=\left(\mathbf{v}^{2}-\mathbf{v}_{0}^{2}\right) /(2 \cdot a) \quad[4,16]
$$

$\mathbf{p}_{1}$ - delay period for the initial step

$$
\begin{equation*}
p_{1}=F /\left(v_{0}^{2}+2 \cdot a\right)^{1 / 2} \tag{17}
\end{equation*}
$$

Ps - delay period for the slew speed steps

$$
\mathbf{p}_{\mathrm{s}}=\mathbf{F} / \mathbf{v}
$$

R - constant multiplier

$$
\mathbf{R}=\mathbf{a} / \mathbf{F}^{2}
$$

The variable delay period $\mathbf{p}$ (initially $\mathbf{p}=\mathbf{p}_{1}$ ) that will be recalculated for each next step is:

$$
\begin{equation*}
p=p \cdot(1+m \cdot p \cdot p) \tag{20}
\end{equation*}
$$

where
$\mathbf{m}$ - variable multiplier that depends on the movement phase:
$\mathbf{m}=-\mathbf{R}$ during acceleration phase,
$\mathbf{m}=0$ between acceleration and deceleration phases, $\mathbf{m}=\mathbf{R}$ during deceleration phase.

For accuracy purpose let's set
$\mathbf{p}=\mathbf{p}_{\mathbf{s}}$ if $\mathbf{p}<\mathbf{p}_{\mathbf{s}}$ or between acceleration and deceleration phases, $p=p_{1}$ if $p>p_{1}$.

## 5. Optional enhancement

Using the higher order approximation of Taylor series

$$
\begin{equation*}
1 /(1+n)^{1 / 2} \simeq 1-n / 2+3 \cdot n^{2} / 8 \tag{21}
\end{equation*}
$$

we can get more accurate results replacing [20] with

$$
p=p \cdot(1+q+1.5 \cdot q \cdot q)
$$

where

$$
q=m \cdot p \cdot p
$$

By [22] we have excellent precision but with two extra multiplications and one extra addition vs [20]'s good precision way. Finally let's construct a very good compromise with just one extra multiplication and one extra addition:

$$
\begin{equation*}
p=p^{\prime}\left(1+q+q^{\prime} q\right) \tag{23}
\end{equation*}
$$

However I think that the good way ([20]) is not merely good but even good enough for most of stepper motor applications.
The enhancement is important for servo drivers with the step/direction control that ramping up from and down to zero speed.

## 6. Programming note

This algorithm was designed for floating point mathematics and in this form it works faster than in the integer form that requires division.

[^0]
[^0]:    * This algorithm was developed by the author in 1994 for L.I.D. Ltd as a part of POEM Stepper Organizer software to control up to 4 axes through IBM PC's parallel port (LPT) and was ported to microcontroller platform in 2004.

    The main field of usage since 1994 - laser diamond cutting.
    ** Special thanks to David Austin [dave@slotech.fsnet.co.uk](mailto:dave@slotech.fsnet.co.uk) who helped me with the enhancement part.

